

Theory of turbocompressors

*A course of lectures. 3 semester.
Group 63238/10*

Department Assistant
Kartashov Sergey, Kozhukhov Yury

Saint-Petersburg Polytechnic University, Department of Compressor, Vacuum and
Refrigeration Engineering

More about compressor technology on the site of
the scientific group www.kviht.com

Theory of turbocompressors. *Lecture 6.*

CONTENT

Turbocompressor's stage theory basics

- The “head” losses schematization when different working modes of the stage by consumption on the example of the impeller: canal losses and inlet losses (shock loss).
- Equation of the sudden expansion losses usage (Bord-Karno equation) for the shock loss calculation.
- Useful “head” characterization.
- Efficiency characterization. Surge limit term. Maximum, critical, optimized and calculated consumptions.
- Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.
- Diffusive flow character. The turbine stage comparison.

Sergey Kartashov, Yuru Kozhukhov Turbocompressors theory.

Lecture 6.

Theoretical “head” coefficient and consumption coefficient dependence when different outlet blades angles.

From the outlet velocity triangles in hypothetical impeller with infinite number of blades

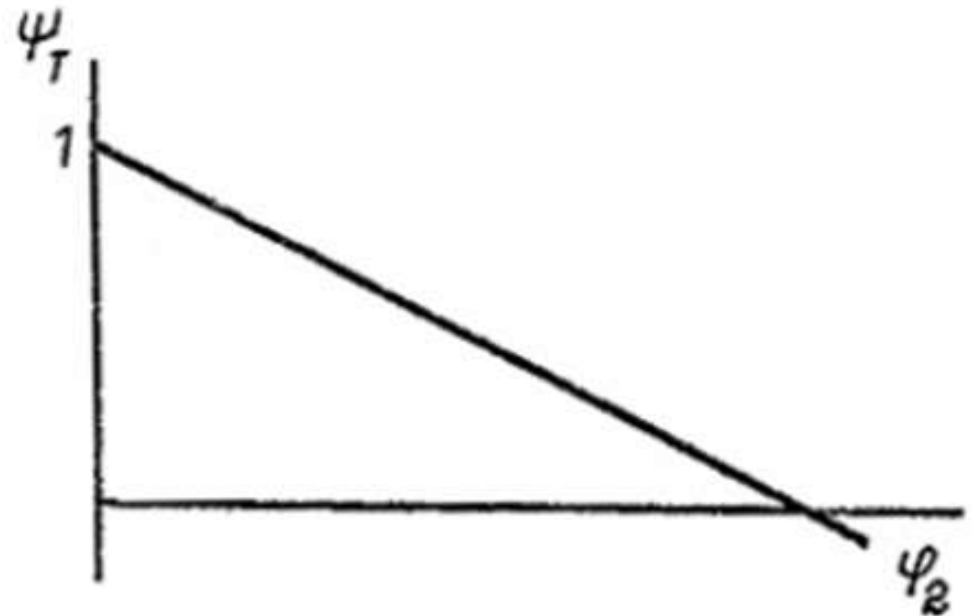
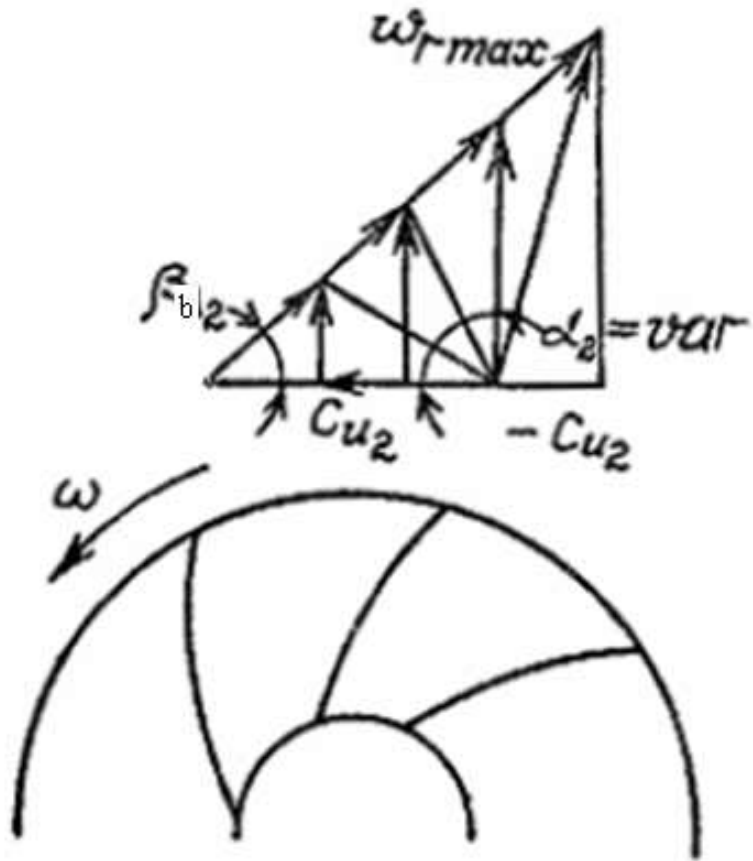
$$c_{u2} = u_2 - w_{u2}$$

$$w_{u2}/w_{r2} = \operatorname{ctg}\beta_{b,2}$$

$$\psi_T = c_{u2}/u_2 = 1 - \varphi_2 \operatorname{ctg}\beta_{b,2}$$

1. $\beta_{b2} < 90^\circ$ (“sweepback blades”)

More about compressor technology on the site of the scientific group www.kviht.com



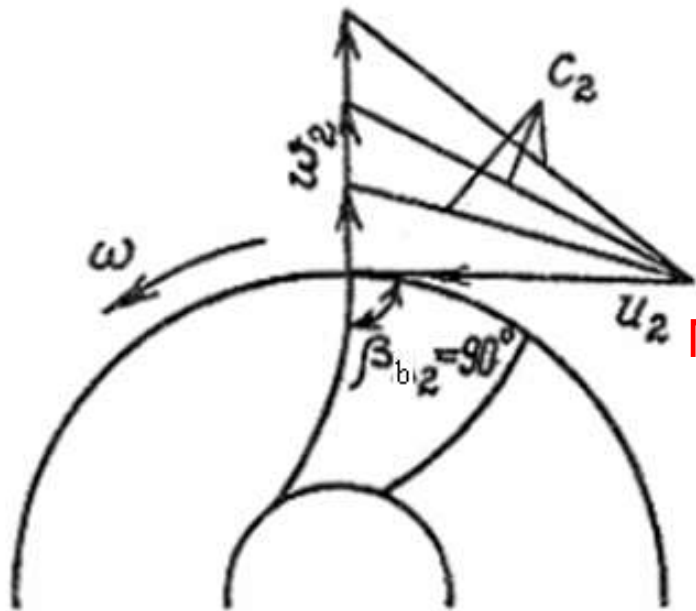
Outlet velocity triangles and “head” characterization of the ideal impeller when infinite blades number $c_{u1}=0$, $\beta_{b2} < 90^\circ$ (“sweepback blades”)

Case when flow with $\varphi_2 > \varphi_{2\max}$ is also practicable. If the characteristics goes from the first to the fourth quadrant, the “head” is negative. Centrifugal compressor is changed to centrifugal turbine, gas is something like “run for” the impeller, “bear against” blade’s back and by “pushing away” from it gets negative swirl.

2. $\beta_{b2}=90^\circ$ (“radial ending blades”)

At this case cotangent of blade’s outlet is equal to zero and “head” coefficient doesn’t depend on consumption

$$\psi_T = f(\varphi_2) = \text{const} = 1$$



More about compressor technology on the site of the scientific group www.kviht.com



Outlet velocity triangles and “head” characteristics of the ideal impeller when infinite number of blades, $c_{u1}=0$, $\beta_{b2}=90^\circ$ (“radial ending blades”)

Lecture 6.

Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.

Degree of reaction Ω – is a ratio between the whole input work in the impeller and it’s part which was used on the gas compression in the impeller. Degree of reaction Ω determines the part of kinetic energy on the impeller outlet.

Lecture 6.

Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.

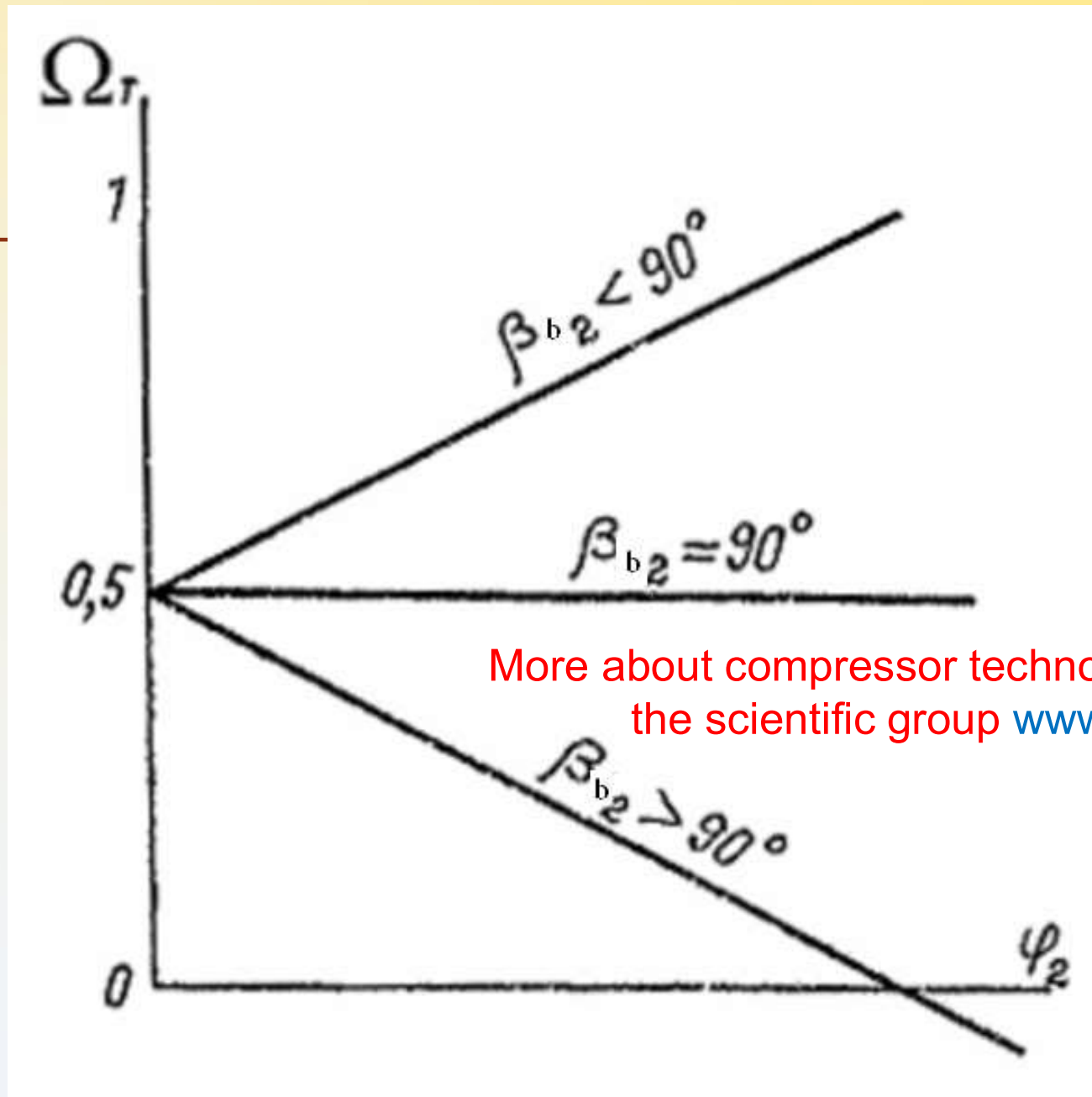
For the ideal impeller with $h_r=0$, $z=\infty$ (when $\beta_2=\beta_{b2}$), $c_{u1}=0$ and when additional condition simplification $c_{r1}=c_{r2}$.

$$\begin{aligned}\Omega_T &= \frac{h_p}{h_T} = \frac{h_T - h_d}{h_T} = 1 - \frac{h_d}{h_T} = \\ &= 1 - 0,5 \frac{c_2^2 - c_1^2}{c_{u2}u_2} = 1 - 0,5 \frac{c_{u2}^2 + c_{r2}^2 - c_{r1}^2}{c_{u2}u_2}\end{aligned}$$

Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.

When $\Omega_T = 1 - 0,5\psi_T$ and $\psi_T = 1 - \varphi_2 \text{ctg}\beta_{b2}$:

$$\Omega_T = 0,5(1 + \varphi_2 \text{ctg}\beta_{b2})$$



Dependence $\Omega = f(\varphi_2)$ when impeller is with $\beta_{b2} > < 90^\circ (z = \infty)$

Lecture 6.

Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.

Pay attention once more that when $c_1=c_{r1}=c_{r2}$ the ratio is:

$$\Omega_T = 1 - 0,5\psi_T,$$

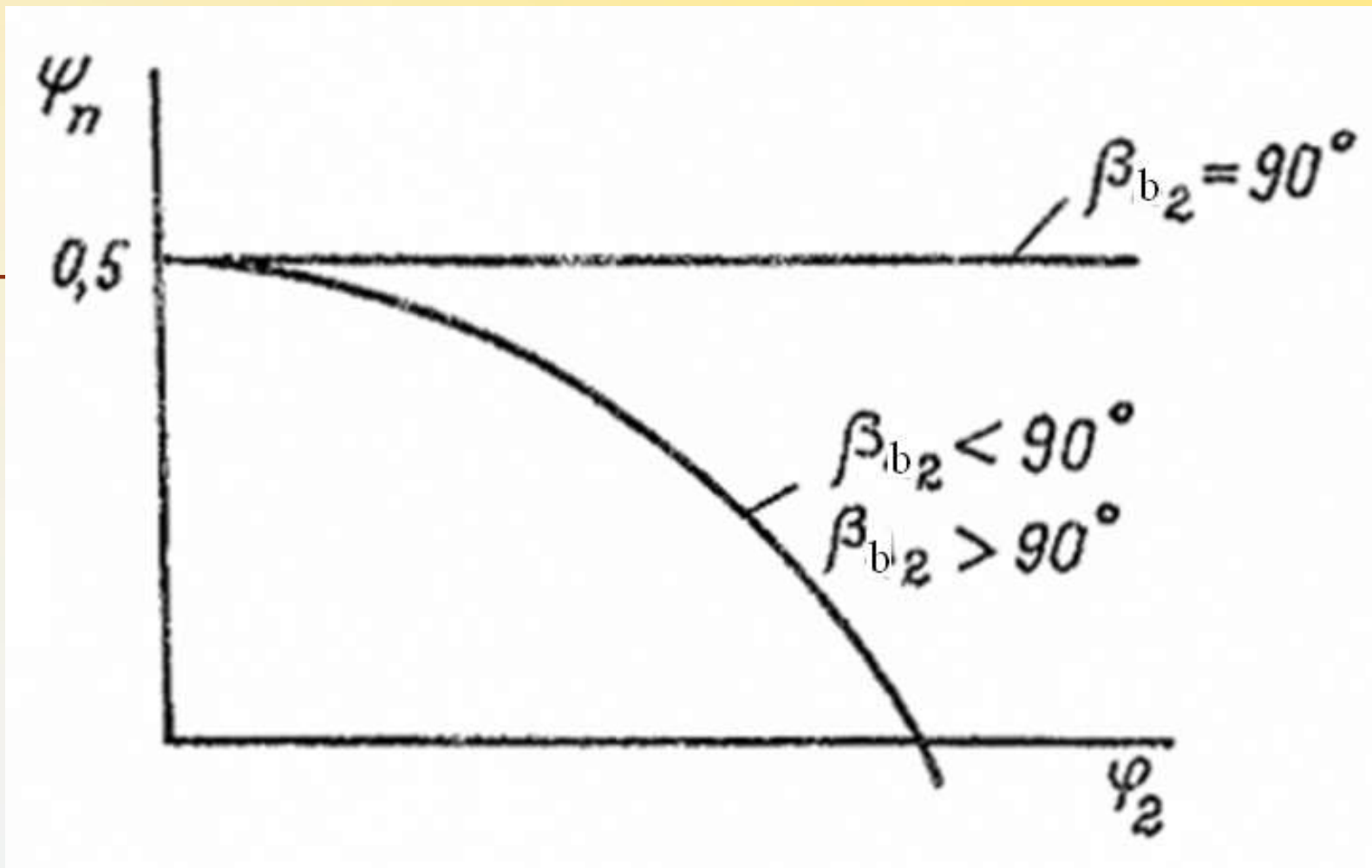
So, the increase of pressure coefficient could be achieved only by decreasing of reaction degree.

Lecture 6.

Degree of reaction. Theoretical “head” coefficient and consumption coefficient dependence when different outlet blade angle. Influence of the blade number finitude.

$$h_{\Pi} = \Omega_T h_T \quad \psi_{\Pi} = \Omega_T \psi_T$$

$$\psi_{\Pi} = 0,5[1 - (\varphi_2 \operatorname{ctg} \beta_{b,2})^2]$$



Static “head” of the impeller and consumption coefficient dependence when different $\beta_{b2} > < 90^\circ$

More about compressor technology on the site of
the scientific group www.kviht.com

The influence of the finite number of blades on the “head” characteristics of the impeller

$$\Psi_T(z = \infty) = 1 - \varphi_2 \operatorname{ctg} \beta_{b2}$$

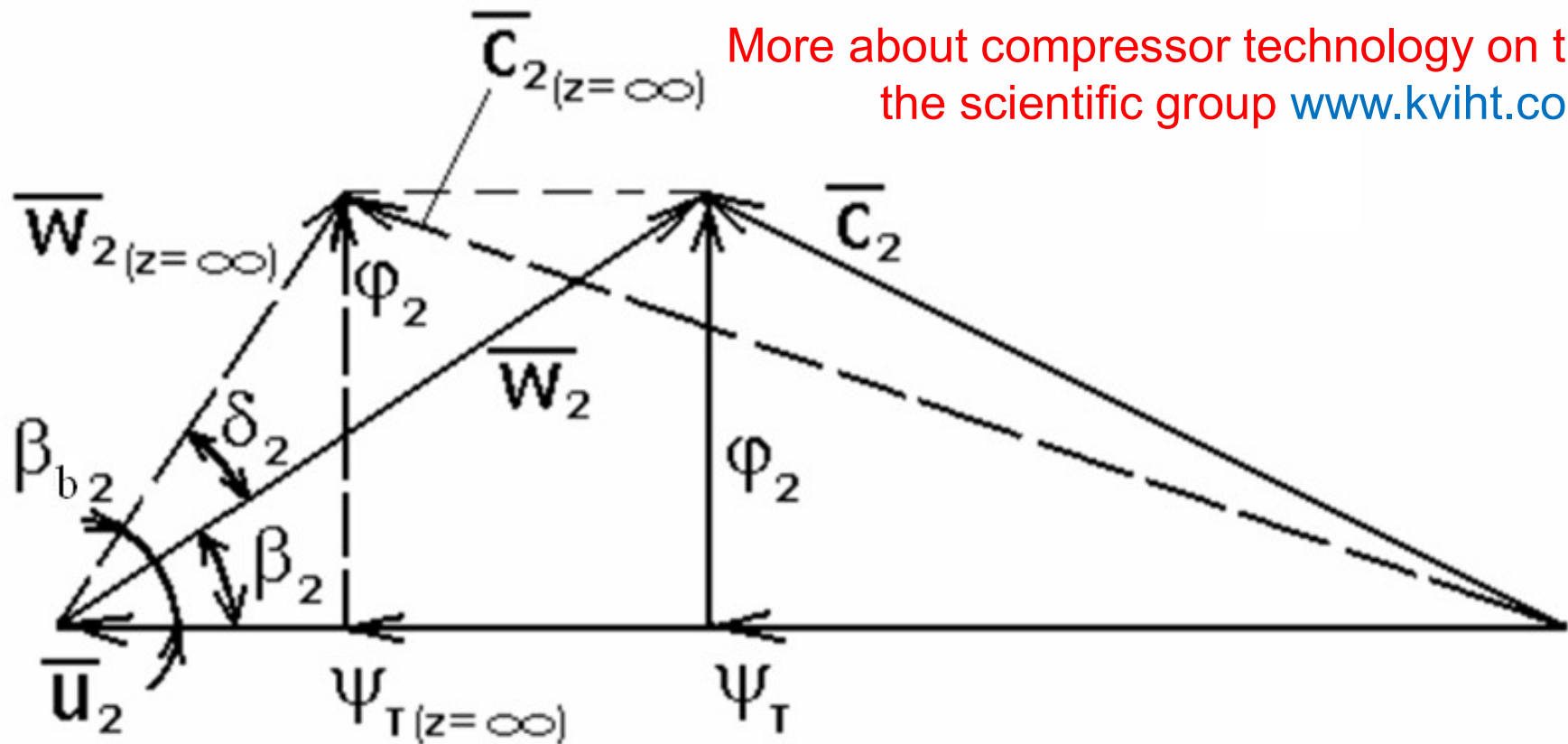
$$\Psi_T = 1 - \varphi_2 \operatorname{ctg} \beta_2 = 1 - \varphi_2 \operatorname{ctg}(\beta_{b2} - \delta_2)$$

Sergey Kartashov, Yuru Kozhukhov Turbocompressors theory.

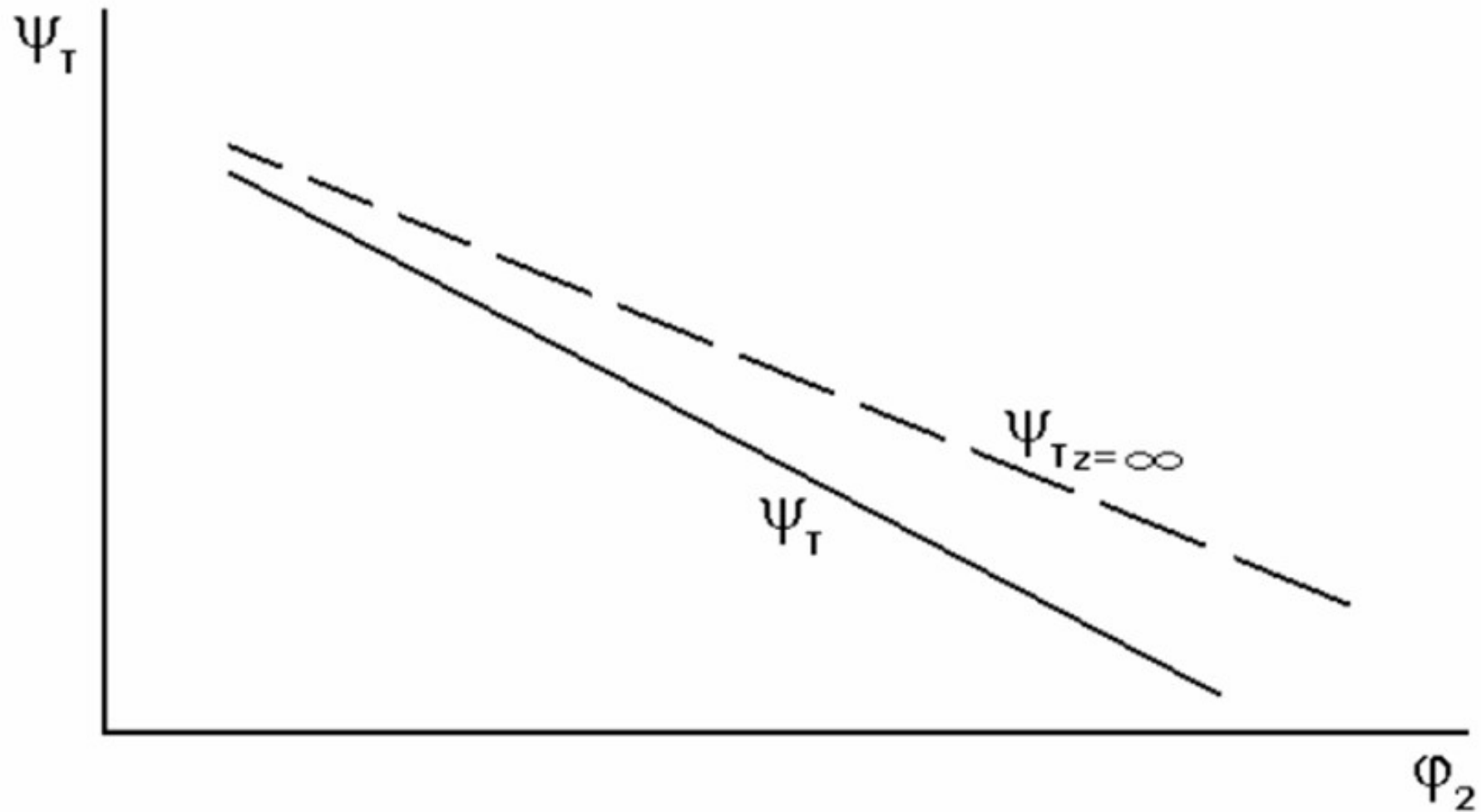
Lecture 6.

The influence of the finite number of blades on the “head” characteristics of the impeller

More about compressor technology on the site of the scientific group www.kviht.com



Velocity triangles for the impeller of centrifugal compressor with infinite blades number (dotted line) and real impeller (solid line)



“Head” characteristics of the impeller of centrifugal compressor with infinite blades number (dotted line) and real impeller (solid line)

More about compressor technology on the site of
the scientific group www.kviht.com

“Head” losses schematization. Bord-Karno equation. Efficiency and useful “head” characteristics.

Centrifugal impeller efficiency:

$$\eta^* = \frac{h_p + h_d}{h_T} = \frac{h_T - h_r}{h_T}$$

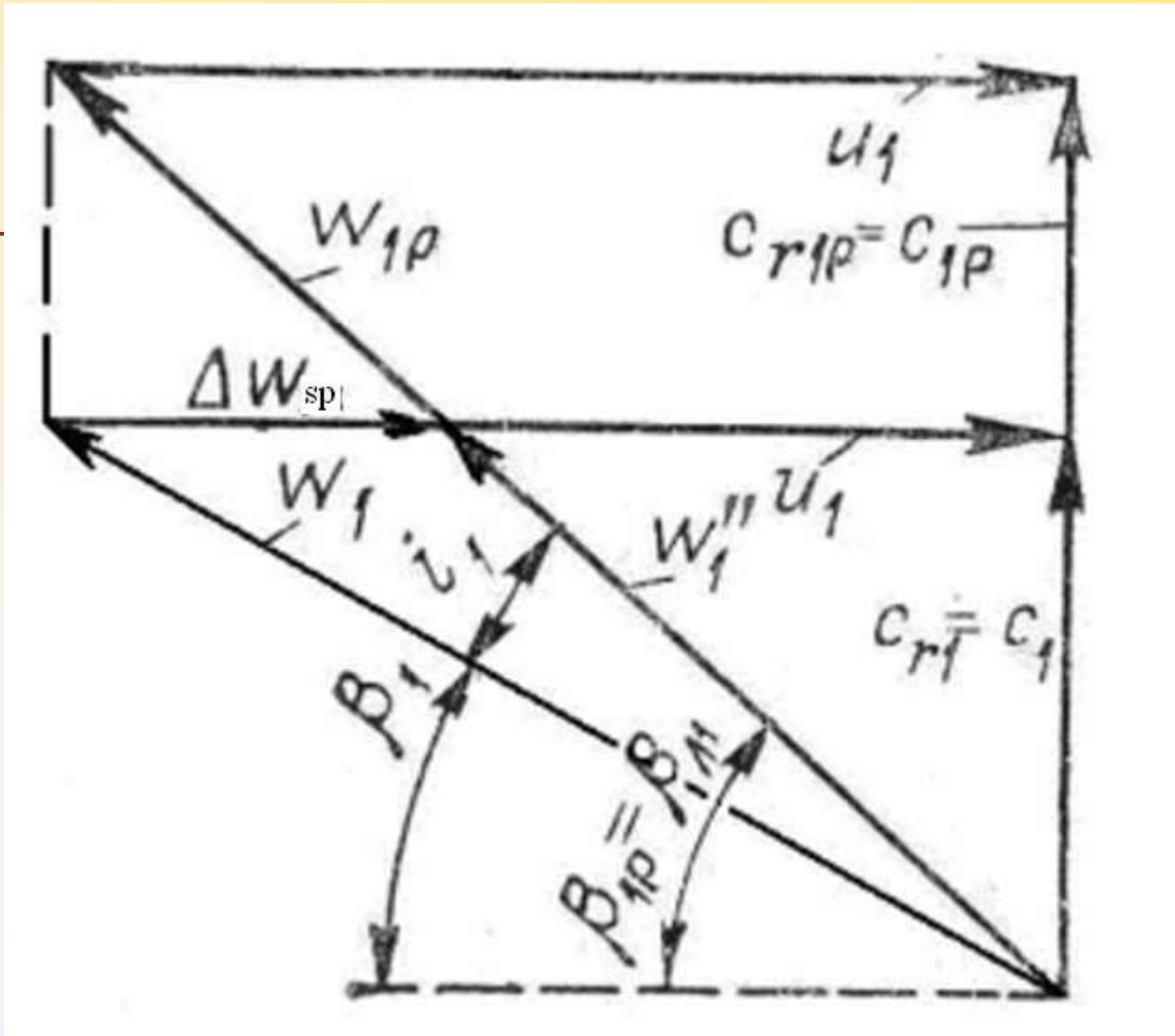
In the first approximation all the losses in the flow passage of the impeller are divided on two groups:

More about compressor technology on the site of
the scientific group www.kviht.com

$$h_r = h_{r\text{ sp}} + h_{r\text{ fr}}$$

The first group of losses – **shock loss $h_{r\ sp}$** – take into account losses which are connected with angle of attack on the blade system inlet in the calculated modes.

The second group of losses **$h_{r\ fr}$** take into account **friction losses** in between blades canals.



More about compressor technology on the site of
the scientific group www.kviht.com

Velocity triangle on the impeller inlet

“Head” losses schematization. Bord-Karno equation. Efficiency and useful “head” characteristics.

Friction losses in between the blades canal is calculated with the help of the formula:

$$h_{r_{fr}} = \zeta_{fr} \frac{w_{1p}^2}{2}, \quad h_{r_{fr}} = \zeta_{fr} \frac{w_{1''}^2}{2}.$$

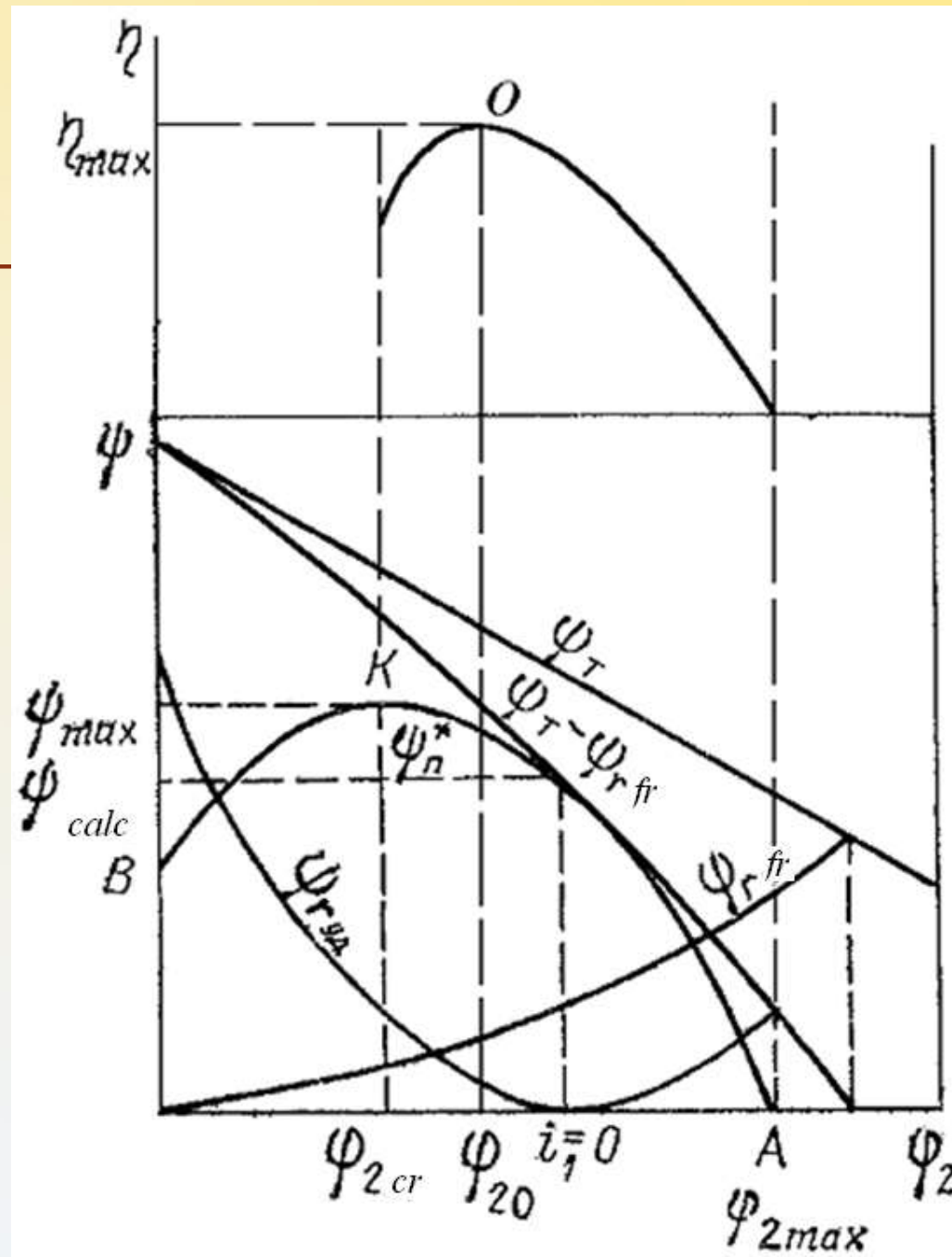
ζ_{fr}

- friction losses coefficient

“Head” losses schematization. Bord-Karno equation. Efficiency and useful “head” characteristics.

Shock losses on not calculated mode will be different from zero. For the shock losses calculation we use **Bord-Karno equation** (the same as sudden expansion losses)

$$h_{r\ sp} = \frac{\Delta w_{sp}^2}{2}$$



More about compressor technology on the site of
the scientific group www.kviht.com

- **Maximum consumption**, when compressor doesn't create the pressure difference – $\varphi_{2\max}$ (dot A).
- **Optimal consumption** φ_{20} corresponds to the efficiency maximum (dot 0).
- **Critical consumption** corresponds to the maximum of useful “head”.
- **Calculated consumption** determined by technical task on the design period, as it is the most time-consuming modes of exploitation.

Surge – is unsteady low frequency process (one period in some seconds), when compressed gas is going to the network and occasionally breaks from network to the inlet

Sergey Kartashov, Yury Kozhukhov Turbocompressors theory.
Lecture 6.

***THANK YOU FOR YOUR
ATTENTION***

More about compressor technology on the site of
the scientific group www.kviht.com